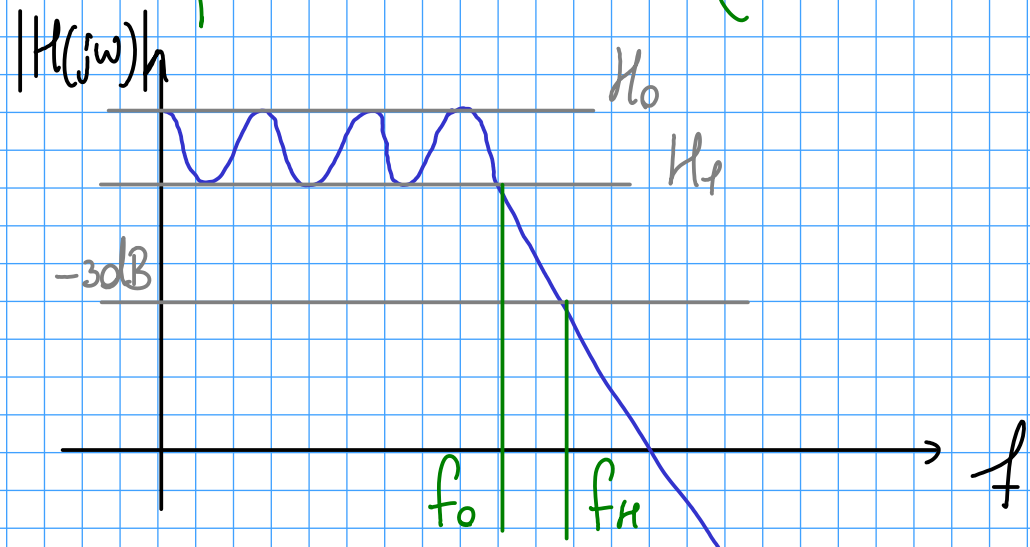


Filtri Chebyshev ellittici

Butterworth \rightarrow risposta piatta in banda passante

Chebyshev \rightarrow oscillazione in banda ma riduco almeno di un grado la complessità rispetto a butterworth (minor costo)

$$|H(j\omega)|^2 = \frac{H_0^2}{1 + \varepsilon^2 C_n^2\left(\frac{\omega}{\omega_c}\right)}$$



$$\text{dove } C_n\left(\frac{\omega}{\omega_c}\right) = \begin{cases} \cos\left[n \cos^{-1}\left(\frac{\omega}{\omega_c}\right)\right] & 0 \leq \frac{\omega}{\omega_c} \leq 1 \\ \cosh\left[n \cosh^{-1}\left(\frac{\omega}{\omega_c}\right)\right] & \frac{\omega}{\omega_c} > 1 \end{cases}$$

$$|H_c(f = f_c)|^2 = \frac{H_0^2}{1 + 5}$$

banda di oscillazione

coeff. su tabelle \rightarrow tabulati per grado di variazione dell'oscillazione

$$\gamma_{dB} = |H_0|_{dB} - |H_1|_{dB} = 20 \log \frac{H_0}{H_1}$$

$$10^{\frac{\gamma}{10}} - 1 = \epsilon^2$$

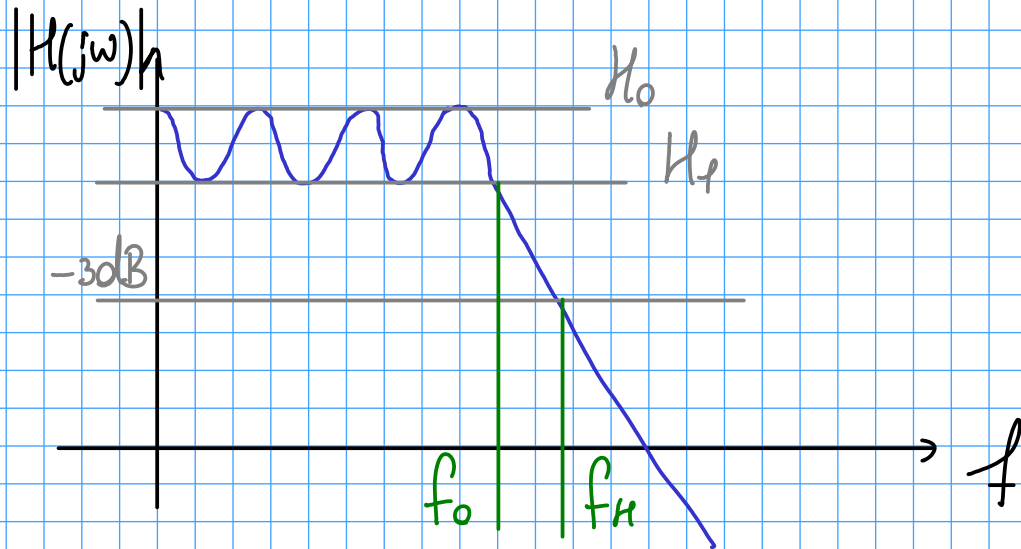
$$\text{con } \gamma = 0,5 \text{ dB} \rightarrow \epsilon = 0,3493$$

$$\text{con } \gamma = 1 \text{ dB} \rightarrow \epsilon = 0,5089$$

banda

in generale
 $f_c \approx f_H$

$$f_H = f_c \cosh \left[\frac{1}{n} \cosh^{-1} (1/\epsilon) \right]$$



esercizio

40 dB su $\frac{\omega}{\omega_c} = 2$

se non ho specifiche stringenti uso
 chebyshev che consente un ordine
 inferiore

confronto butterworth / chebyshev (con $\delta = 1 \text{ dB}$)

$$\frac{|H(j\omega)|^2}{|H_0|^2} = \frac{1}{1 + \epsilon^2 C_n^2 \left(\frac{\omega}{\omega_c} \right)} = \frac{1}{1 + \epsilon^2 C_n^2 2} = 10^{-4}$$

$$1 + \epsilon^2 C_n^2(2) = 10^{+4} \rightarrow C_n^2(2) = \frac{10^4}{(0,5089)^2} = 38,613 \cdot 10^3$$

$$\delta = 1 \text{ dB} \rightarrow \epsilon = 0,5089$$

$$C_n(2) = 196,49$$

$$C_n(2) = \cosh[n \cosh^{-1}(2)] \rightarrow n = 4,53 \rightarrow n = 5$$

ordine polinomio 5

$$f_n = 1,034 f_c \approx f_c$$

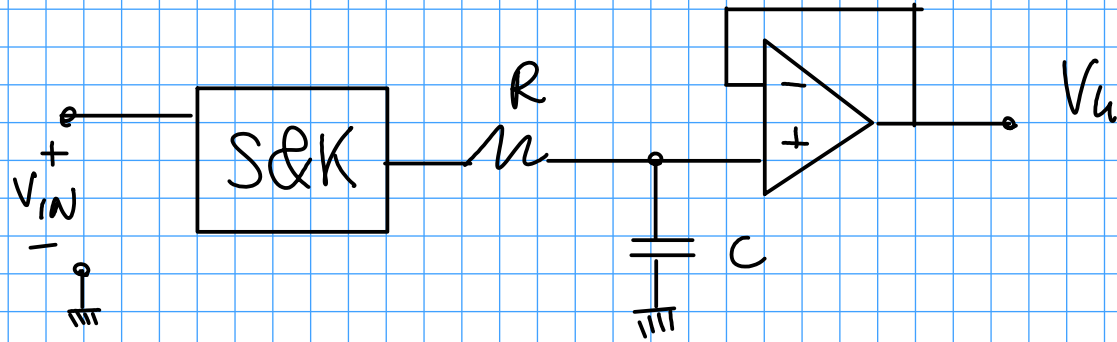
rediamo butterworth

$$\frac{|H(j\omega)|}{|H_0|} = \frac{1}{\sqrt{\left(\frac{\omega}{\omega_c}\right)^{2n} + 1}} \rightarrow \frac{1}{\sqrt{\left(\frac{\omega}{\omega_c}\right)^{2n} + 1}} = 10^{-4}$$

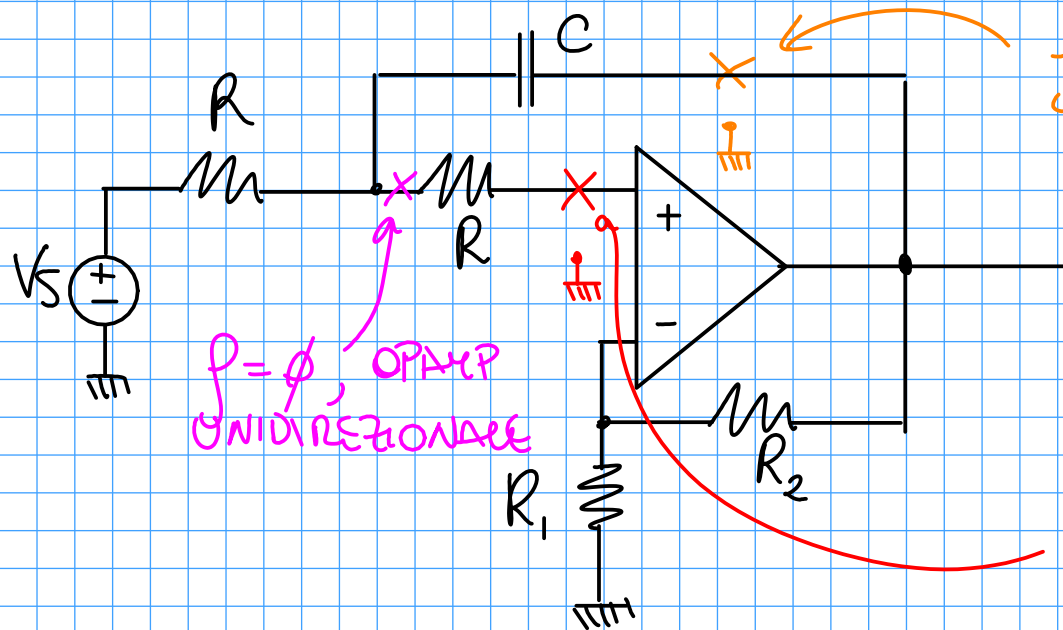
$$\left(\frac{\omega}{\omega_c}\right)^{2n} = 10^4 - 1 \rightarrow 4^n = 10^4 \rightarrow \underline{\underline{n = 7}}$$

con butterworth $\rightarrow 7^\circ$ grado!

seppuriamo $n=3$, come lo realizzo?

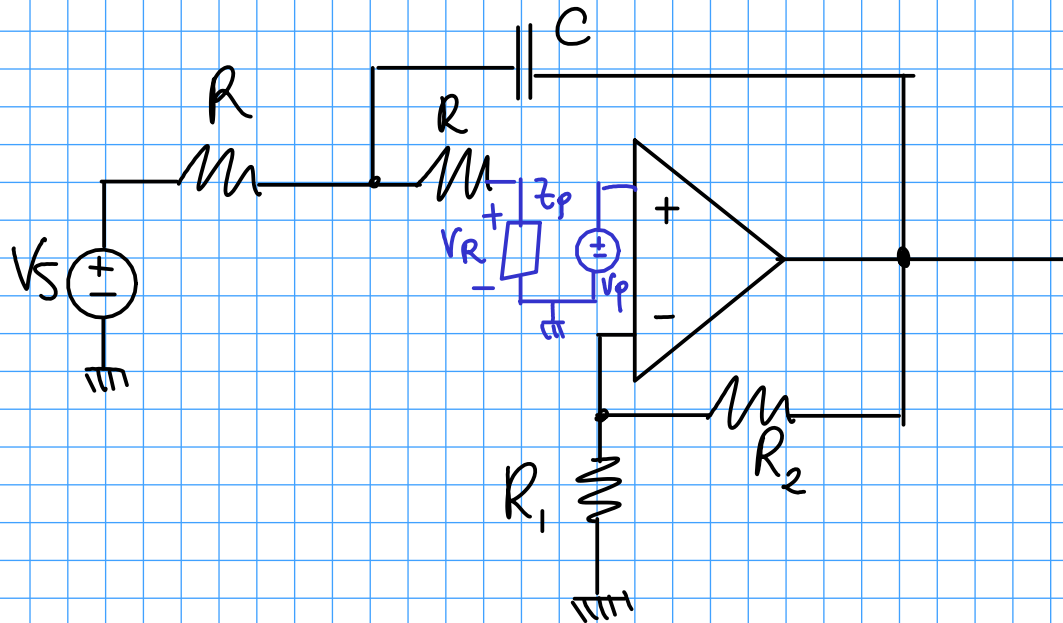


cello di Sallen & Key



$f \neq 0$, HA z_p NON INFWISCE

$f = \phi$ USIAMO QUESTO



$$f = \phi, \quad \delta = \left. \frac{v_y}{v_s} \right|_{v_p = \phi} = \phi$$

$$A_f = \frac{\alpha A}{1 - \beta A}$$

$$A = \left. \frac{v_y}{v_p} \right|_{v_s = \phi} = 1 + \frac{R_2}{R_1}$$

$$\alpha = \left. \frac{v_R}{v_s} \right|_{v_p = \phi}$$

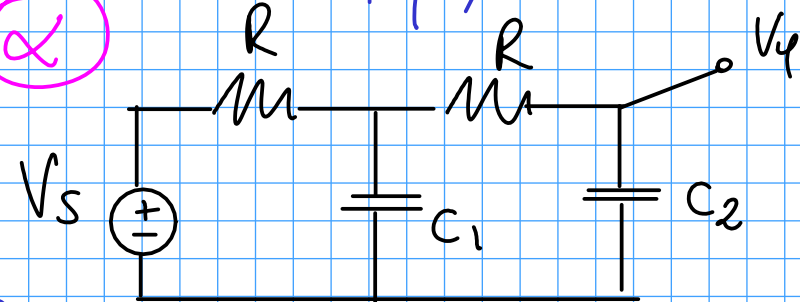
$$\alpha(f) = \frac{\alpha_0}{Q_2 s^2 + a_1 s + 1}$$

$$a_1 = R_{11}^0 C_1 + R_{22}^0 C_2 = RC_1 + 2RC_2 = 3RC$$

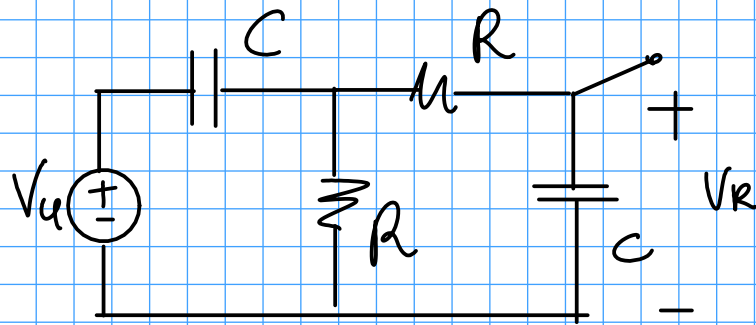
$$a_2 = C_1 C_2 R_{11}^0 R_{22}^1 = C_1 C_2 R R = R^2 C^2$$

$$\alpha = \frac{1}{R^2 C^2 s^2 + 3RCs + 1}$$

α



③

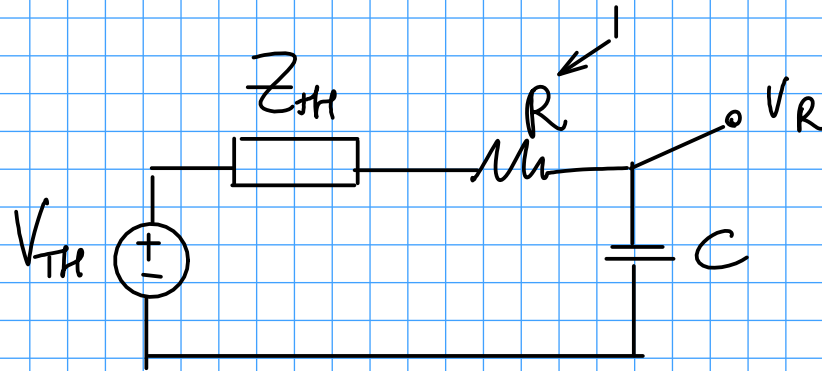


$$\beta = \frac{K_s}{R^2 C^2 s^2 + 3RCs + 1}$$

come α

ZERO non'online

CALCOLO ZERO \rightarrow CIRCUITO C₁

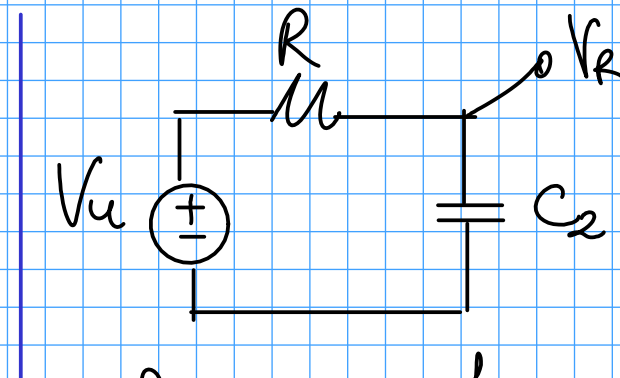


$$V_{TH} = V_u \frac{R}{R + \frac{1}{Cs}}$$

$$Z_{TH} = \frac{R}{RCs + 1}$$

se $s \rightarrow +\infty$
$V_{TH} \rightarrow V_u$
$Z_{TH} \rightarrow \emptyset$

Al limite vero
circolo significato



$$\beta_{\infty} = \frac{1}{RCs + 1}$$

con $s \rightarrow +\infty$

$$\left. \frac{V_R}{V_u} \right|_{s \rightarrow \infty} = \frac{\frac{1}{Cs}}{\frac{1}{Cs} + R}$$

$$\beta = \frac{Ks}{R^2C^2s^2 + 3RCs + 1}$$

$$\beta_{\infty} = \frac{1}{RCs}$$

$$\frac{1}{RCs} = \frac{K}{R^2C^2s} \implies K = RC$$

$$\beta = \frac{RC}{R^2C^2s^2 + 3RCs + 1}$$

$$A_f = \frac{\alpha A}{1 - \beta A} = \frac{A_0}{R^2 C^2 s^2 + 3RCs + 1 - A_0 RCs}$$

$$A_f = \frac{A_0}{R^2 C^2 s^2 + RCs(3 - A_0) + 1}$$

GRADO 2 \rightarrow REGOLA NEWTON \rightarrow POLI A PARTE REALE POSITIVA
QUANTE SONO LE VALUTAZIONI
DI SEGNO

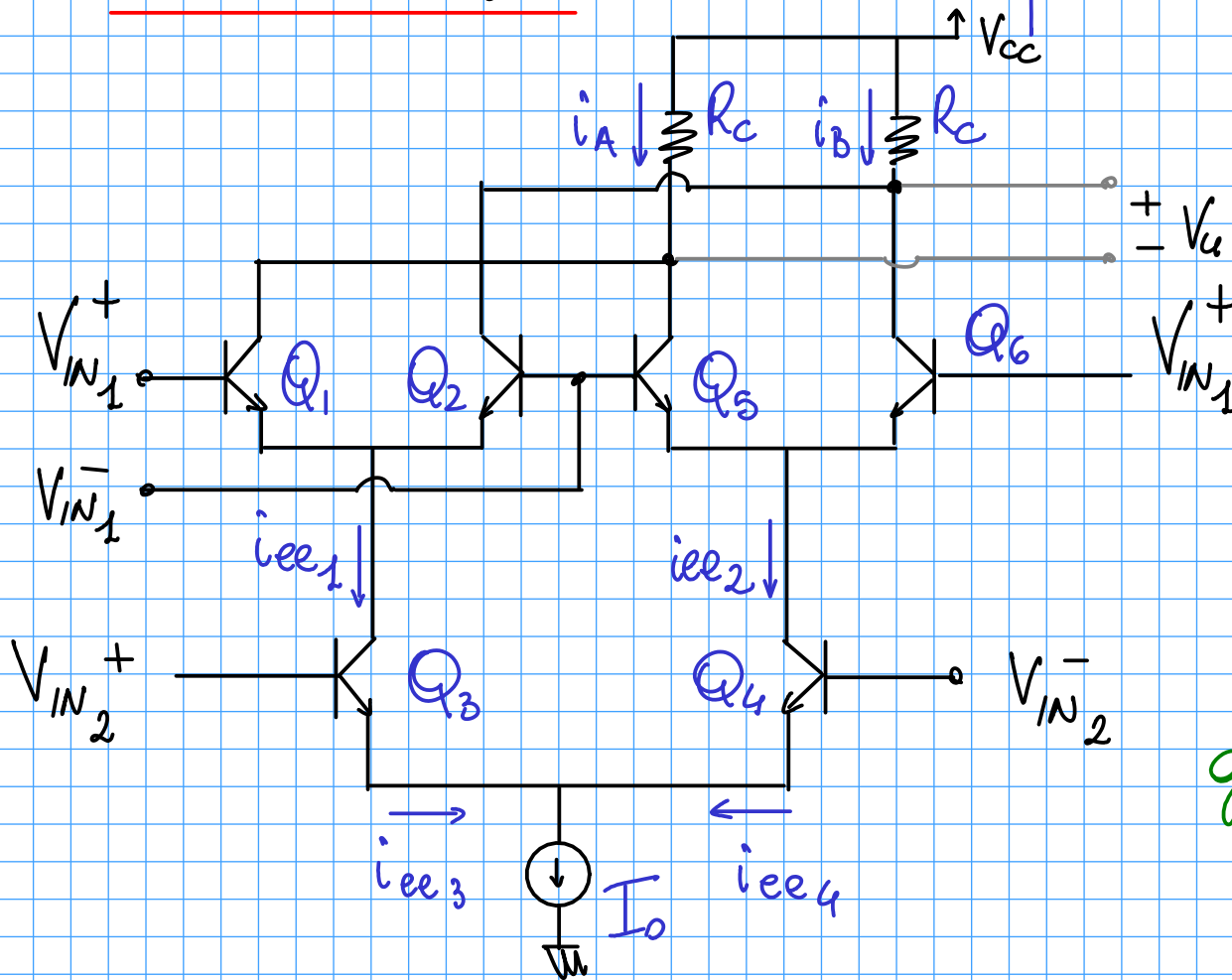
GRADO SUP \rightarrow " RAUTH

\rightarrow STABILE $\rightarrow 3 - A_0 > 0 \Rightarrow \underline{A_0 < 3}$

\rightarrow SE VOGLIO A MAGGIORE \rightarrow USO ALTRO AMP. IN CASCATA

Cella di Gilbert

→ moltiplicazioni a 4 quadranti



polarizzazione

$$I_{EE1} = I_{EE2} = \frac{I_0}{2}$$

valore totale (riposo + variazioni)

$$\begin{cases} i_{EE1} = g_{m3} \frac{V_{IN2}}{2} \\ i_{EE2} = -g_{m4} \frac{V_{IN2}}{2} \end{cases}$$

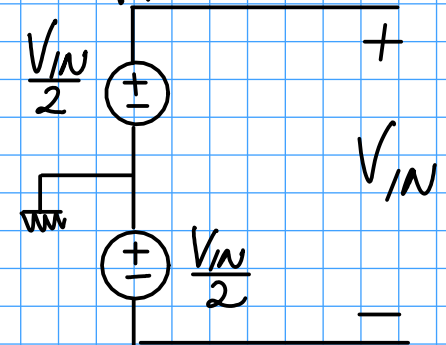
$$g_{m3} = g_{m4} = \frac{I_0}{2V_T}$$

sostituisco g_m →

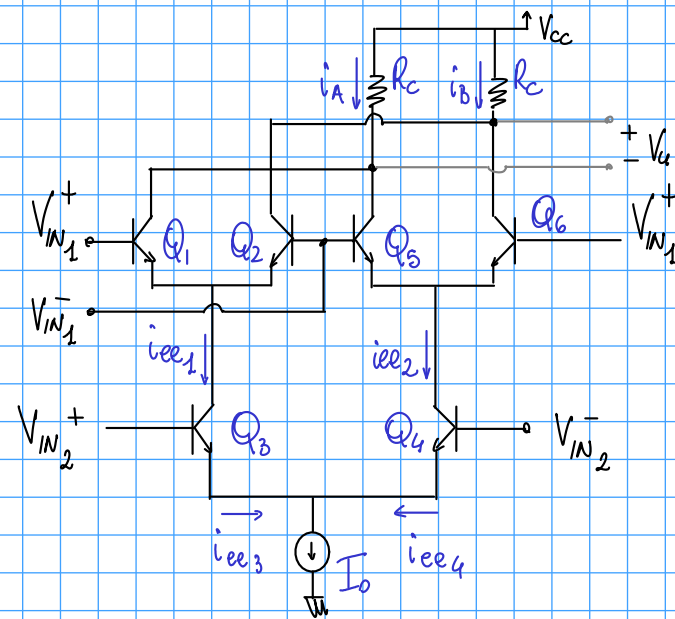
$$\begin{cases} i_{EE1} = + \frac{I_0}{2V_T} \frac{V_{IN2}}{2} \\ i_{EE2} = - \frac{I_0}{2V_T} \frac{V_{IN2}}{2} \end{cases}$$

$g_m = \frac{I_c}{V_T}$

sviluppo:



$$\begin{cases} i_A = i_{c1} + i_{c5} \\ i_B = i_{c6} + i_{c2} \end{cases}$$



$$i_{c1} = \frac{i_{EE1}}{2} + g_{m1} \frac{V_{IN1}}{2}$$

$$i_{c5} = \frac{i_{EE2}}{2} - g_{m5} \frac{V_{IN1}}{2}$$

$$i_{c6} = \frac{i_{EE2}}{2} + g_{m6} \frac{V_{IN1}}{2}$$

$$i_{c2} = \frac{i_{EE1}}{2} - g_{m2} \frac{V_{IN1}}{2}$$

con $g_{m1} = g_{m2}$, $g_{m5} = g_{m6}$

calcolo uscita

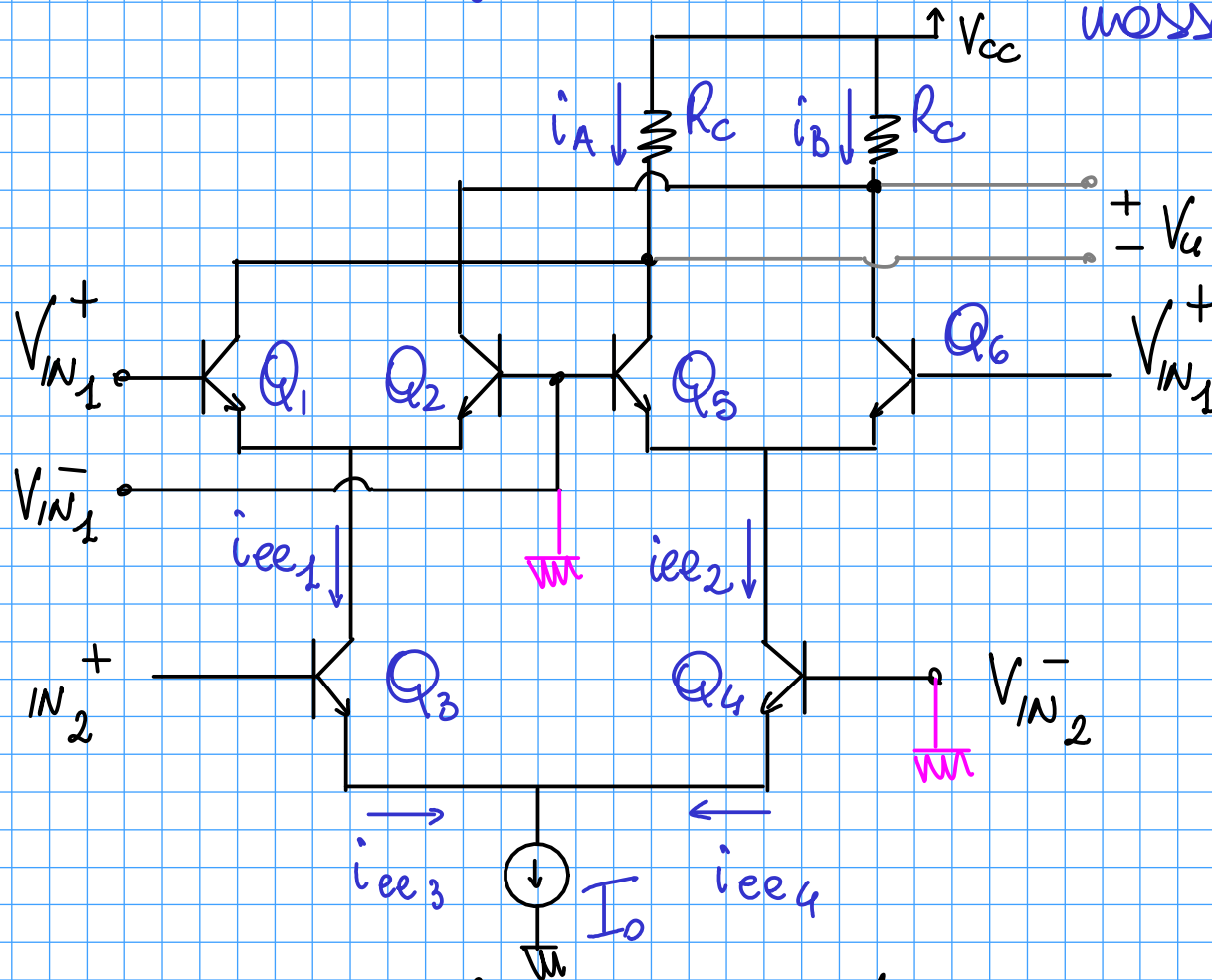
$$\begin{aligned} V_u &= (V_{CC} - R_c i_B) - (V_{CC} - R_c i_A) = R_c (i_A - i_B) = R_c (g_{m1} - g_{m6}) V_{IN} = \\ &= R_c \left(\frac{i_{EE1}}{2V_T} - \frac{i_{EE2}}{2V_T} \right) V_{IN} = \frac{R_c}{2V_T} \left(\frac{I_o}{2V_T} \right) V_{IN1} V_{IN2} \rightarrow \boxed{V_u = K V_{IN1} V_{IN2}} \end{aligned}$$

moltiplicatore

riscrivo i_A e i_B con le relazioni trovate

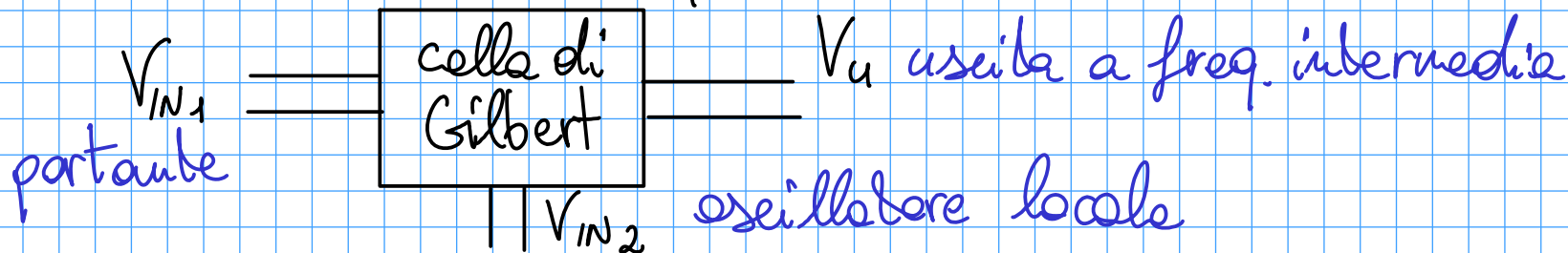
$$\begin{cases} i_A = \frac{i_{EE1}}{2} + g_{m1} \frac{V_{IN1}}{2} + \frac{i_{EE2}}{2} - g_{m5} \frac{V_{IN1}}{2} \\ i_B = \frac{i_{EE2}}{2} + g_{m6} \frac{V_{IN1}}{2} + \frac{i_{EE1}}{2} - g_{m2} \frac{V_{IN1}}{2} \end{cases}$$

limite : ingressi non possono essere forniti con riferimento a massa, ma diffenziali



altrimenti i transistor dei terminali "-" entrano in saturazione o interdizione

se ingressi forniti in modo differenziale il sistema lavora correttamente, fino ad ampiezze dell'ordine di V_T

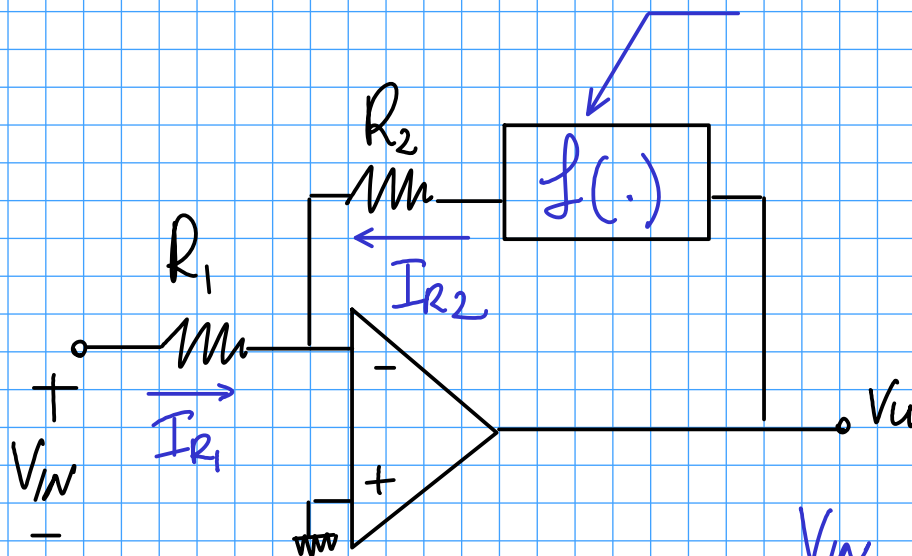
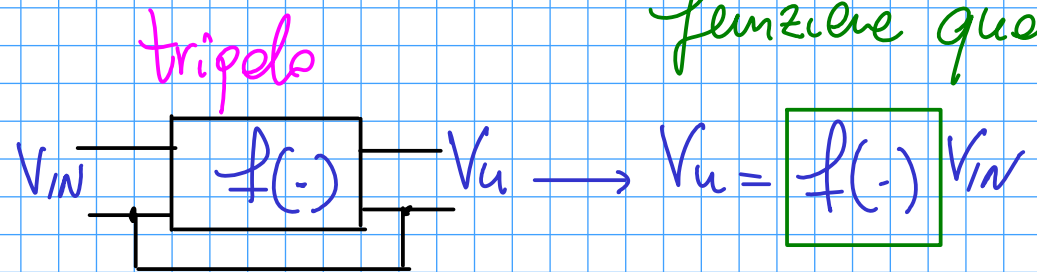


anche
come
mixer

utilizzi celle di Gilbert

premessa: utilizzo della retroazione per realizzare l'inverso di una qualsiasi funzione $f(\cdot)$ implementata da un blocco inserito nella catena di retroazione

funzione qualsiasi



$$I_{R1} = -I_{R2} \text{ (coro circuito virtuale)}$$

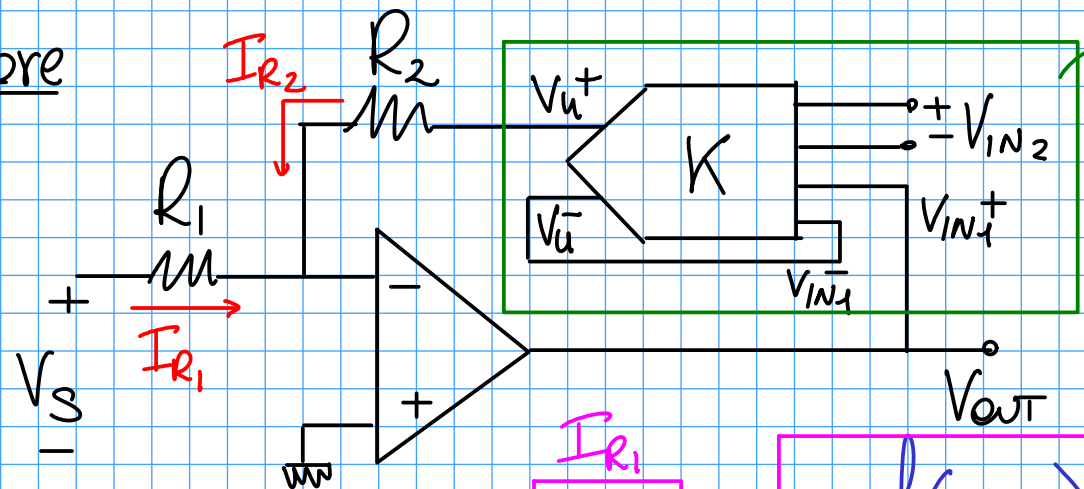
$$I_{R1} = \frac{V_{IN}}{R_1}, \quad I_{R2} = \frac{f(V_u)}{R_2}$$

$$\frac{V_{IN}}{R_1} = -\frac{f(V_u)}{R_2} \rightarrow V_u = \underline{\underline{f^{-1} \left[-\frac{R_2}{R_1} V_{IN} \right]}}$$

otengo l'inverso in uscita!

vediamo se posso utilizzare una cella di Gilbert per realizzare un divisore, secondo questa "filosofia" -----

divisore



cella di Gilbert
implementata
 $V_u = K V_{IN_1} V_{IN_2}$

$$I_{R_1} = -I_{R_2}$$

$$\frac{V_S}{R_1} = - \frac{I(V_{OUT})}{R_2}$$

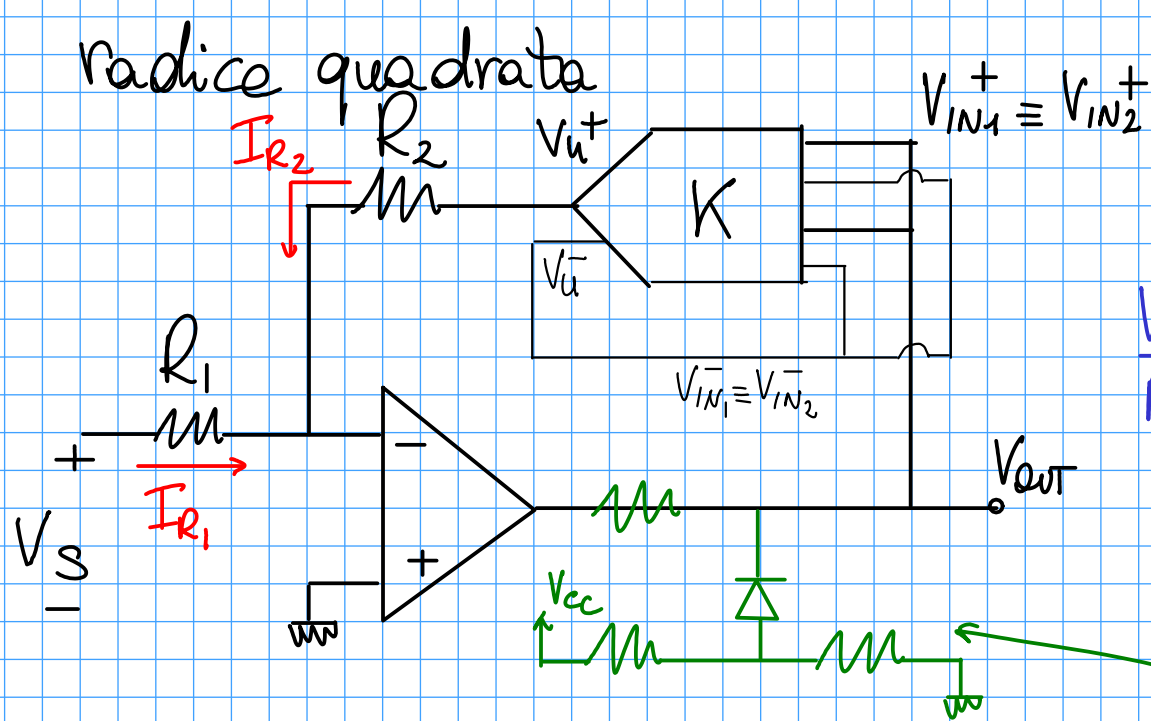
$$V_{OUT} = - \frac{1}{K} \frac{R_2}{R_1} \frac{V_S}{V_{IN_2}}$$

$$I(V_{OUT}) = K V_{IN_2} V_{OUT}$$

limite:

con $V_{IN_2} \sim \phi$ operazionale satura (come fosse open loop)

radice quadrata



$$\frac{V_{in2}}{R_1} = -\frac{V_u^2}{KR_2}$$

$$\frac{V_S}{R_1} = -\frac{f(V_{out})}{R_2} = -\frac{KV_{out}^2}{R_2}$$

$$f(V_{out}) = KV_{out}^2$$

$$V_{out} = \pm \sqrt{-V_S K \frac{R_2}{R_1}}$$

V_S deve essere negativa, altrimenti saturazione
operazionale

$V_{out} > 0$, altrimenti ho retroazione
positiva

impongo con circuito esterno